

## TIME MULTIPLEX PLL STEREO DECODER

### GENERAL DESCRIPTION

The TDA1578A is a PLL stereo decoder based on the time-division multiplex principle.

#### Features

- adjustable input and output voltage levels
- automatic mono/stereo switching with hysteresis, controlled by both pilot signal and field strength level
- analogue control of mono/stereo change over
- pilot indicator driver
- analogue muting control
- muting indicator driver
- oscillator with decoupled frequency measurement output
- electronic smoothing of the supply voltage

### QUICK REFERENCE DATA

Measured with a frequency deviation  $\Delta f = \pm 75$  kHz without pilot;  $f_m = 1$  kHz

Supply voltage (pin 8)	$V_P = V_{8-7}$	typ.	8,5		15	V
Supply current (pin 8)	$I_P = I_8$	typ.	21		30	mA
Multiplex input signal (adjustable)	$V_{MUX(p-p)}$	typ.	0,5		1	V
Input resistance (adjustable)	$R_i$	typ.	47			k $\Omega$
A.F. output voltage ( $R = 15$ k $\Omega$ )	$V_o$	typ.	0,75		1,5	V
Output resistance	$R_o$					low-ohmic
Spread in gain	$\Delta G_V$	$\leq$			1	dB
Channel separation	$\alpha$	typ.			50	dB
Total harmonic distortion	THD	$\leq$	0,3		0,1	%
Signal-to-noise ratio	S/N	typ.			90	dB
Carrier and harmonic suppression						
pilot signal; $f = 19$ kHz	$\alpha_{19}$	typ.			32	dB
subcarrier; $f = 38$ kHz	$\alpha_{38}$	typ.			50	dB
$f = 57$ kHz	$\alpha_{57}$	typ.			46	dB
$f = 76$ kHz	$\alpha_{76}$	typ.			60	dB
traffic radio (V.W.F.); $f = 57$ kHz	$\alpha_{57(VWF)}$	typ.			70	dB
SCA (Subsidiary Communications Authorization); $f = 67$ kHz	$\alpha_{67}$	typ.			70	dB
ACI (Adjacent Channel Interference); $f = 114$ kHz	$\alpha_{114}$	typ.			80	dB
intermodulation; $f = 10/13$ kHz	$\alpha_2, \alpha_3$	typ.			70	dB
Supply voltage range (pin 8)	$V_P = V_{8-7}$		7,5 to 18			V
Operating ambient temperature range	$T_{amb}$		-30 to + 80			$^{\circ}C$

### PACKAGE OUTLINE

18-lead DIL; plastic (SOT102).

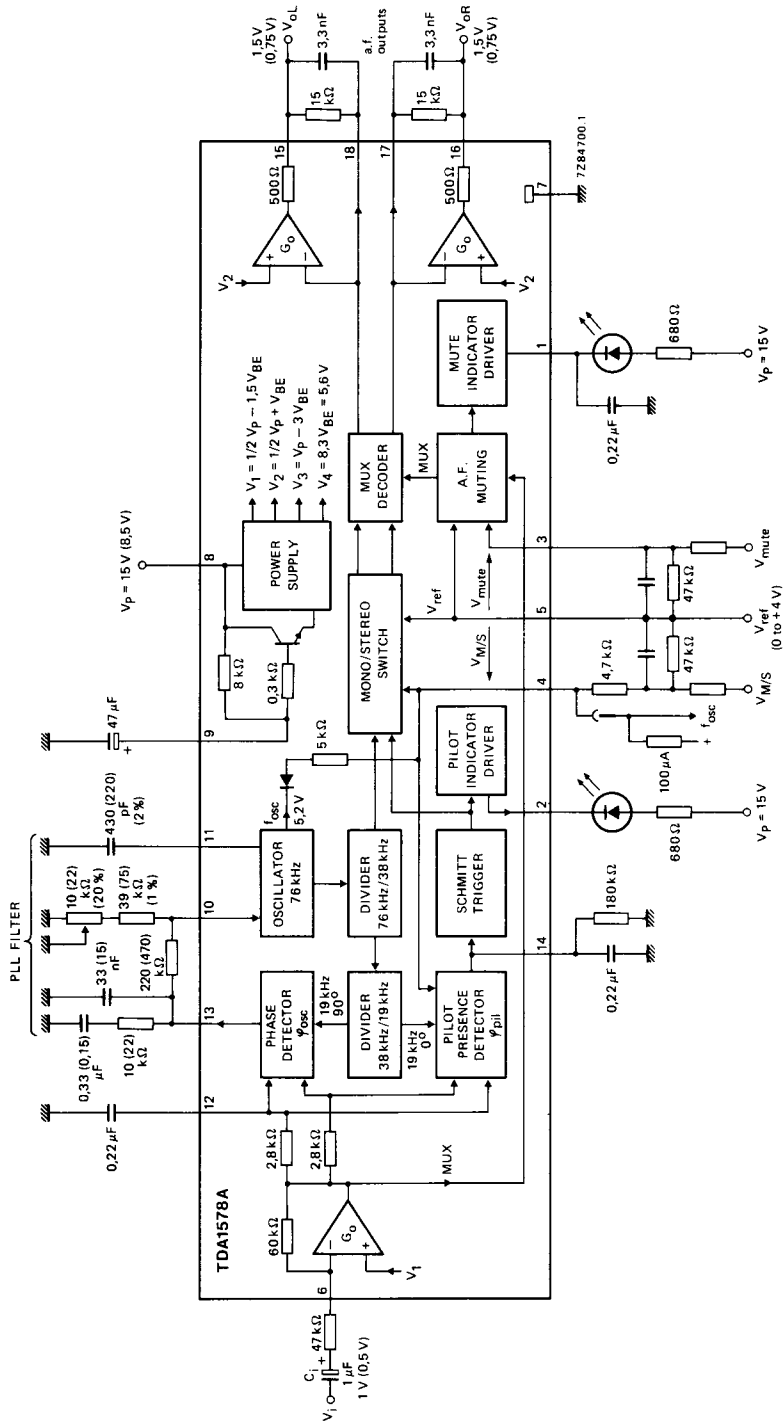


Fig. 1 Block diagram with external components; used as test circuit. Values given in parentheses are for  $V_p = 8,5$  V.

**RATINGS**

Limiting values in accordance with the Absolute Maximum System (IEC 134)

Supply voltage (pin 8)	$V_p = V_{8-7}$	max.	20 V
Input voltages (pins 3, 4 and 5)	$V_{3;4;5-7}$		0 to 12 V
Indicator driver output voltage	$V_{1;2-7}$	max.	24 V
Indicator driver output current	$I_1; I_2$	max.	30 mA
Total power dissipation at $T_{amb} = 25\text{ }^\circ\text{C}$	$P_{tot}$	max.	1,2 W
Storage temperature range	$T_{stg}$		-55 to + 150 $^\circ\text{C}$
Operating ambient temperature range	$T_{amb}$		-30 to + 80 $^\circ\text{C}$

**THERMAL RESISTANCE**

From crystal to ambient	$R_{th\ c-a}$	=	80 K/W
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## CHARACTERISTICS (measured in Fig. 1)

Input signal:  $m = 100\%$  ( $\Delta f = \pm 75$  kHz); pilot signal:  $m = 9\%$  ( $\Delta f = \pm 6,75$  kHz);modulation frequency: 1 kHz;  $V_{3-5} = V_{4-5} = 0$  V;de-emphasizing time:  $T = 50$   $\mu$ s; oscillator adjusted to  $f_{OSC}$  at a pilot voltage  $V_i = 0$  V; $T_{amb} = 25$  °C; unless otherwise specified

parameter	V <sub>p</sub> (V)	symbol	min.	typ.	max.	unit
Supply voltage range (pin 8)	—	V <sub>p</sub>	7,5	—	18	V
Supply current (except output and indicator) pin 8	8,5	I <sub>p</sub>	—	21	—	mA
	15	I <sub>p</sub>	—	30	40	mA
Nominal multiplex input voltage (peak-to-peak value) R <sub>i</sub> = 47 k $\Omega$	8,5	V <sub>MUX(p-p)</sub>	—	0,5	—	V
	15	V <sub>MUX(p-p)</sub>	—	1,0	—	V
Overdrive reserve of input at THD = 1 % at THD = 0,3 %	8,5		3	6	—	dB
	15		3	6	—	dB
A.F. output voltage (r.m.s. value; mono without pilot) R <sub>15-18</sub> = R <sub>16-17</sub> = 15 k $\Omega$	8,5	V <sub>O(rms)</sub>	—	0,75	—	V
	15	V <sub>O(rms)</sub>	—	1,5	—	V
R <sub>15-18</sub> = R <sub>16-17</sub> = 24 k $\Omega$	8,5	V <sub>O(rms)</sub>	—	1,2	—	V
	15	V <sub>O(rms)</sub>	—	2,4	—	V
Overdrive reserve of output R <sub>15-18</sub> = R <sub>16-17</sub> = 24 k $\Omega$	*		3	—	—	dB
Spread in output voltage levels	*	$\pm \Delta V_O/V_O$	—	—	1	dB
Difference of output voltage levels	*	$\pm \Delta V_{15-16}/V_O$	—	—	1	dB
Output resistance	*	R <sub>O</sub>	low-ohmic			
Available output current pins 15 and 16	*	$\pm I_O$	—	—	—	mA
Modulation range at output (unloaded)	*	V <sub>15;16-7</sub>	—	1 to V <sub>g.7-1</sub>	—	V
Internal current limiting	*	I <sub>O</sub>	—	15	—	mA
D.C. output voltage R <sub>15-18</sub> = R <sub>16-17</sub> = 24 k $\Omega$	8,5	V <sub>15;16-7</sub>	3,6	4,1	4,6	V
	15	V <sub>15;16-7</sub>	7,0	7,7	8,4	V
D.C. current (pins 17 and 18)	8,5	-I <sub>17;18</sub>	—	33	—	$\mu$ A
	15	-I <sub>17;18</sub>	—	23	—	$\mu$ A

\* V<sub>p</sub> = 8,5 or 15 V.

parameter	V <sub>p</sub> (V)	symbol	min.	typ.	max.	unit
Channel separation at V <sub>4.5</sub> = 0 V	8,5	$\alpha$	32	50	—	dB
	15	$\alpha$	39	50	—	dB
Total harmonic distortion	8,5	THD	—	0,1	0,3	%
	15	THD	—	0,04	0,1	%
Signal-to-noise ratio f = 20 Hz to 16 kHz	8,5	S/N	—	87	—	dB
	15	S/N	—	90	—	dB
Carrier and harmonic suppression at the output						
pilot signal; f = 19 kHz	*	$\alpha_{19}$	—	32	—	dB
subcarrier; f = 38 kHz	*	$\alpha_{38}$	40	50	—	dB
f = 57 kHz	*	$\alpha_{57}$	—	46	—	dB
f = 76 kHz	*	$\alpha_{76}$	—	60	—	dB
intermodulation (note 1)						
f <sub>m</sub> = 10 kHz; spurious signal f <sub>s</sub> = 1 kHz PLL-filter Fig. 1	*	$\alpha_2$	—	50	—	dB
PLL-filter Fig. 2	*	$\alpha_2$	—	70	—	dB
f <sub>m</sub> = 13 kHz; spurious signal f <sub>s</sub> = 1 kHz	*	$\alpha_3$	—	75	—	dB
traffic radio (V.W.F.); f = 57 kHz (note 2)	*	$\alpha_{57(VWF)}$	—	70	—	dB
SCA (Subsidiary Communi- cations Authorization); f = 67 kHz (note 4)	*	$\alpha_{67}$	—	70	—	dB
ACI (Adjacent Channel Interference) (note 3); f = 114 kHz	*	$\alpha_{114}$	—	80	—	dB
f = 190 kHz	*	$\alpha_{190}$	—	52	—	dB
Ripple rejection at the output; f = 100 Hz; V <sub>p(rms)</sub> = 100 mV (pin 8)	*	RR <sub>100</sub>	40	43	—	dB
Voltage on filter capacitor without external load	*	V <sub>9.7</sub>	—	V <sub>p-0,25</sub>	—	V
Source resistance	*	R <sub>9.8</sub>	6	8	10	k $\Omega$

\* V<sub>p</sub> = 8,5 or 15 V.

## CHARACTERISTICS (continued)

parameter	V <sub>p</sub> (V)	symbol	min.	typ.	max.	unit
<b>Mono/stereo control</b>						
Pilot threshold voltages (peak-to-peak values) for stereo 'ON'	8,5	V <sub>i(p-p)</sub>	—	21	30	mV
	15	V <sub>i(p-p)</sub>	—	43	61	mV
for mono 'ON'	8,5	V <sub>i(p-p)</sub>	6	15	—	mV
	15	V <sub>i(p-p)</sub>	12	30	—	mV
Switch hysteresis V <sub>i ON</sub> /V <sub>i OFF</sub>	*	ΔV <sub>i</sub>	—	3	—	dB
Switching time at C <sub>14.7</sub> = 0,22 μF for stereo 'ON'	*	t <sub>st ON</sub>	—	15	—	ms
	*	t <sub>m ON</sub>	—	27	—	ms
<b>External mono/stereo control</b> (see Fig. 12 and note 5)						
Switching voltage for external mono control	8,5	V <sub>14.7</sub>	—	—	0,7	V
	15	V <sub>14.7</sub>	—	—	1,4	V
	*	or: -V <sub>4.5</sub>	315	—	—	mV
Control voltage for channel separation: α = 6 dB	8,5	-V <sub>4.5</sub>	—	120	—	mV
	15	-V <sub>4.5</sub>	—	130	—	mV
	*	ΔV <sub>4.5</sub>	—	—	± 20	mV
α = 26 dB	8,5	-V <sub>4.5</sub>	—	70	—	mV
	15	-V <sub>4.5</sub>	—	80	—	mV
Control voltage for mono 'ON'	8,5	-V <sub>4.5</sub>	—	240	—	mV
	15	-V <sub>4.5</sub>	—	270	—	mV
for stereo 'ON'	8,5	-V <sub>4.5</sub>	—	220	—	mV
	15	-V <sub>4.5</sub>	—	250	—	mV
Control voltage difference for α = 6 dB; stereo 'ON'	8,5	ΔV <sub>4.7</sub>	80	100	120	mV

\* V<sub>p</sub> = 8,5 or 15 V.

parameter	V <sub>P</sub> (V)	symbol	min.	typ.	max.	unit
<b>Muting circuit</b> (see Fig. 13 and note 5)						
Control voltage for an attenuation: $\alpha = 3$ dB	8,5	$-V_{3-5}$	—	140	—	mV
	15	$-V_{3-5}$	—	145	—	mV
$\alpha = 26$ dB	*	$\Delta V_{3-5}$	—	$\pm 20$	—	mV
	8,5	$-V_{3-5}$	—	255	—	mV
	15	$-V_{3-5}$	—	270	—	mV
<b>Attenuation</b>						
with $V_{3-5} = 0$ V	*	$\alpha$	—	—	0,2	dB
with $-V_{3-5} = 450$ mV	*	$\alpha$	—	80	—	dB
<b>LED driver output current at an attenuation: <math>\alpha = 3</math> dB</b>						
	*	$I_1$	1,2	1,7	2,2	mA
<b>Control voltage</b>						
for $I_1 = 200$ $\mu$ A	8,5	$-V_{3-5}$	—	150	—	mV
	15	$-V_{3-5}$	—	160	—	mV
<b>Control inputs</b>						
<b>Recommended voltage range</b>						
	*	$V_{3;4;5-7}$	0	—	4	V
<b>Input bias current</b>						
	*	$I_{3;4;5}$	—	10	100	nA
<b>Indicator driver</b>						
<b>Output saturation voltages</b>						
at $I_1 = 20$ mA; $V_{3-5} = 0$ V	*	$V_{1-7sat}$	—	1,2	1,8	V
at $I_2 = 20$ mA	*	$V_{2-7sat}$	—	0,5	1,0	V
<b>Output leakage current</b>						
at $V_{1;2-7} = 24$ V	*	$I_{1;2}$	—	20	—	$\mu$ A

\* V<sub>P</sub> = 8,5 or 15 V.

## CHARACTERISTICS (continued)

parameter	V <sub>p</sub> (V)	symbol	min.	typ.	max.	unit
<b>VCO</b>						
Oscillator frequency adjustable with R <sub>10-7</sub>	*	f <sub>osc</sub>	—	76	—	kHz
Spread of free-running frequency at nominal external circuitry	*	f <sub>osc</sub>	71	—	82	kHz
Free-running frequency dependency (note 6) with temperature	*	TC	—	1 x 10 <sup>-4</sup>	—	K <sup>-1</sup>
with supply voltage	*	Δf <sub>osc</sub> /ΔV <sub>p</sub>	—	—	400	Hz/V
Capture and holding range for a pilot input voltage V <sub>pil</sub> = 0,5 x V <sub>pil nom</sub>	*	Δf/f	± 2	—	—	%
PLL control slope (total)	*	S <sub>tot</sub>	—	4,5	—	kHz/μs
D.C. voltage at pin 10	*	V <sub>10-7</sub> or:	—	2,1 3,2 V <sub>BE</sub>	—	V V
Frequency measuring point; internal switching threshold	*	V <sub>4-7</sub> or:	—	6 9 V <sub>BE</sub>	—	V V
Output voltage (peak-to-peak value) at pin 4; R = 4,7 kΩ	*	V <sub>4-7(p-p)</sub>	—	350	—	mV
Output resistance	*	R <sub>4-7</sub>	—	5	—	kΩ

\* V<sub>p</sub> = 8,5 or 15 V.



**Notes to the characteristics**

1. Intermodulation suppression (BFC: Beat-Frequency Components)

$$\alpha_2 = \frac{V_{O(\text{signal})} \text{ (at 1 kHz)}}{V_{O(\text{spurious})} \text{ (at 1 kHz)}}; f_s = (2 \times 10 \text{ kHz}) - 19 \text{ kHz}$$

$$\alpha_3 = \frac{V_{O(\text{signal})} \text{ (at 1 kHz)}}{V_{O(\text{spurious})} \text{ (at 1 kHz)}}; f_s = (3 \times 13 \text{ kHz}) - 38 \text{ kHz}$$

measured with: 91% mono signal;  $f_m = 10$  or  $13$  kHz; 9% pilot signal.

2. Traffic radio (V.W.F.) suppression

$$\alpha_{57(\text{VWF})} = \frac{V_{O(\text{signal})} \text{ (at 1 kHz)}}{V_{O(\text{spurious})} \text{ (at 1 kHz} \pm 23 \text{ kHz)}}$$

measured with: 91% stereo signal;  $f_m = 1$  kHz; 9% pilot signal;  
5% traffic subcarrier ( $f = 57$  kHz,  $f_m = 23$  Hz AM,  $m = 60\%$ ).

3. ACI (Adjacent Channel Interference)

$$\alpha_{114} = \frac{V_{O(\text{signal})} \text{ (at 1 kHz)}}{V_{O(\text{spurious})} \text{ (at 4 kHz)}}; f_s = 110 \text{ kHz} - (3 \times 38 \text{ kHz})$$

$$\alpha_{190} = \frac{V_{O(\text{signal})} \text{ (at 1 kHz)}}{V_{O(\text{spurious})} \text{ (at 4 kHz)}}; f_s = 186 \text{ kHz} - (5 \times 38 \text{ kHz})$$

measured with: 90% mono signal;  $f_m = 1$  kHz; 9% pilot signal;  
1% spurious signal ( $f_s = 110$  or  $186$  kHz, unmodulated).

4. SCA (Subsidiary Communications Authorization)

$$\alpha_{67} = \frac{V_{O(\text{signal})} \text{ (at 1 kHz)}}{V_{O(\text{spurious})} \text{ (at 9 kHz)}}; f_s = (2 \times 38 \text{ kHz}) - 67 \text{ kHz}$$

measured with: 81% mono signal;  $f_m = 1$  kHz; 9% pilot signal;  
10% SCA-subcarrier ( $f_s = 67$  kHz, unmodulated).

5. Assuming
- $V_T = \frac{k \times T}{q} = 28,6$
- mV at
- $T_j = 330$
- K.

6. The effects of external components are not taken into account.

**APPLICATION NOTES**

1. When mono/stereo control and muting control are not used, pins 3, 4 and 5 have to be grounded.
2. In a receiver, channel separation adjustment can be obtained by:
  - a. A capacitor at pin 12 ( $C_{12-7}$ ): phasing 19/38 kHz
  - b. RC or LCR filter at the input: frequency response compensation ( $V_G = f(\omega)$ )
  - c. Feeding the output signals of the output amplifier to the inputs of the other channel.
3. PLL-filter for reduced intermodulation ( $\alpha_2$ ); see Fig. 2.
4. External mono 'ON' switch; see Fig. 3.
5. Switching 'OFF' the oscillator; see Fig. 4.

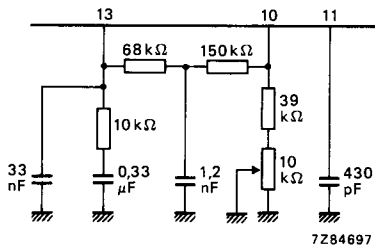


Fig. 2 PLL-filter for  $\alpha_2 = 70$  dB at  $V_P = 15$  V (see also Fig. 1).

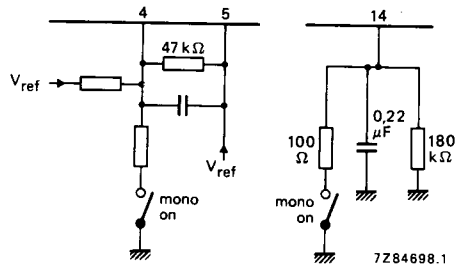


Fig. 3 (a) At pin 4;  $-V_{4-5} > 300$  mV; (b) at pin 14.

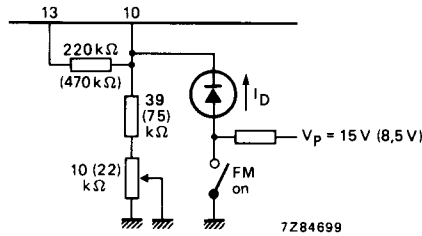


Fig. 4 The oscillator is switched-off when:  $I_D > 100 \mu A$  ( $> 50 \mu A$  for  $V_P = 8,5$  V) and  $I_D < 1$  mA.

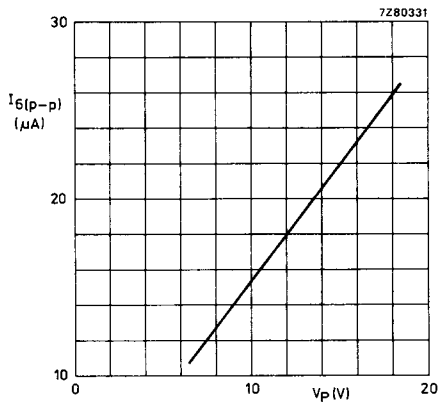


Fig. 5 Signal handling range at the input for  $I_{6nom}$  ( $\pm 75$  kHz);  $V_{g.7} = V_p$ .

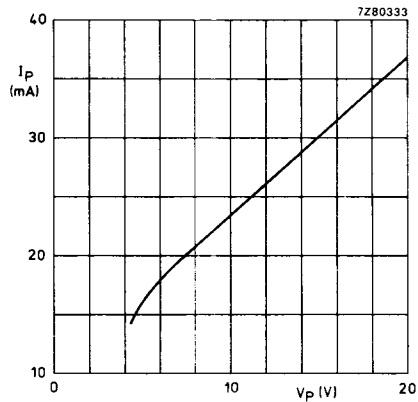


Fig. 6 Supply current consumption at  $V_{g.7} = V_p$ .

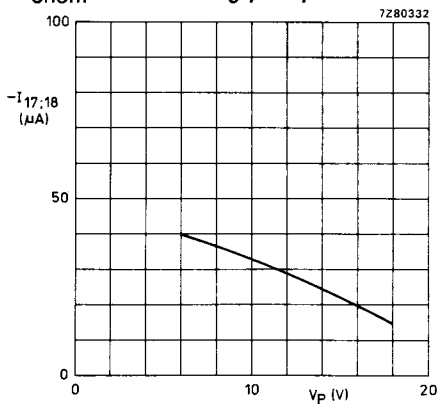


Fig. 7 D.C. current in the feedback loop of the output amplifier.

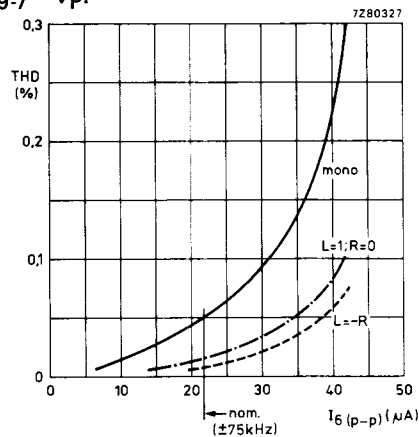


Fig. 8 Total harmonic distortion (THD) as a function of the peak-to-peak input current at pin 6;  $V_p = 15$  V;  $f_m = 1$  kHz;  $V_{3.5} = V_{4.5} = 0$  V.

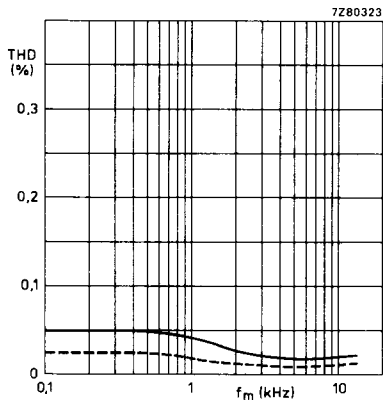


Fig. 9 Total harmonic distortion (THD) as a function of the modulation frequency ( $f_m$ );  $V_p = 15$  V;  $I_{6(p-p)} = 21,5$   $\mu$ A.

— mono  
 - - - stereo;  $L = -R$ ; 91% + 9% pilot signal.

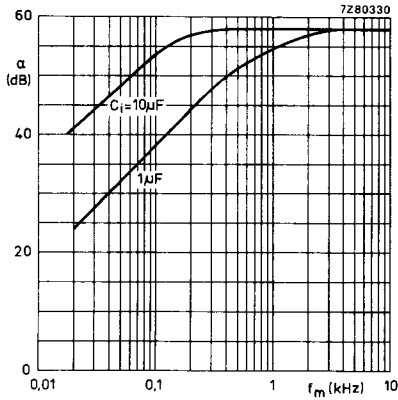


Fig. 10 Channel separation ( $\alpha$ ) as a function of the modulation frequency ( $f_m$ );  $V_p = 15 V$ ;  $R_i = 47 k\Omega$ ;  $V_{4-5} = 0 V$ .

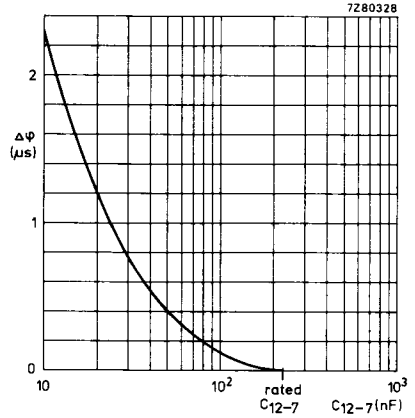


Fig. 11 Phase shift between pilot signal at the input and the internal carrier processing as a function of  $C_{12-7}$ .

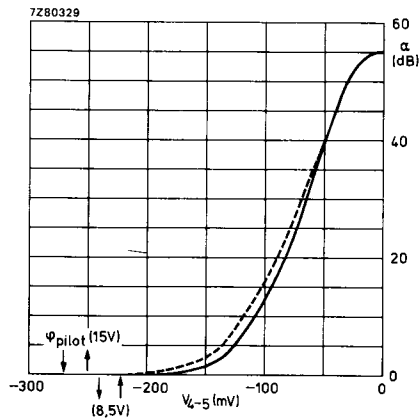


Fig. 12 Mono/stereo control at  $f_m = 1 kHz$ ;  $\alpha$  is the channel separation.

—  $V_p = 8,5 V$   
 - - -  $V_p = 15 V$

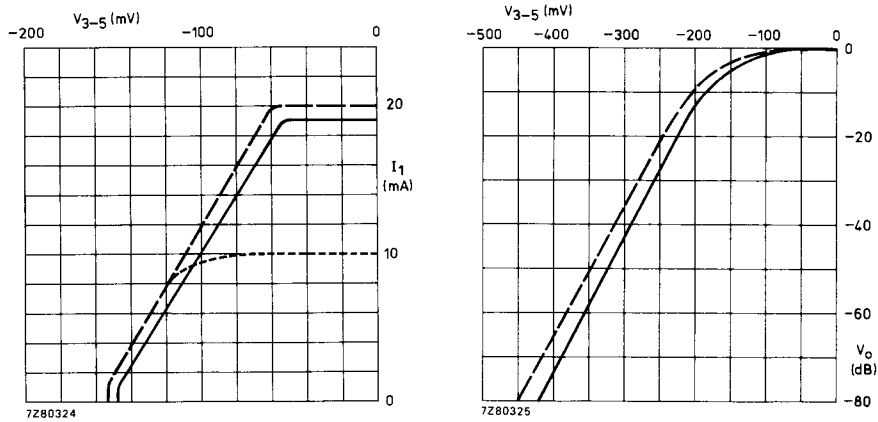


Fig. 13 Muting ( $V_o$ ) and muting indicator current ( $I_1$ ) as a function of  $V_{3-5}$ .

$V_o$  in dB curves; ———  $V_p = 8,5$  V

-----  $V_p = 15$  V

$I_1$  in mA curves for  $V_{PL}/R_{bias1}$  (pin 1); - - - - 22 V/1 k $\Omega$

———— 14 V/680  $\Omega$

----- 10 V/680  $\Omega$

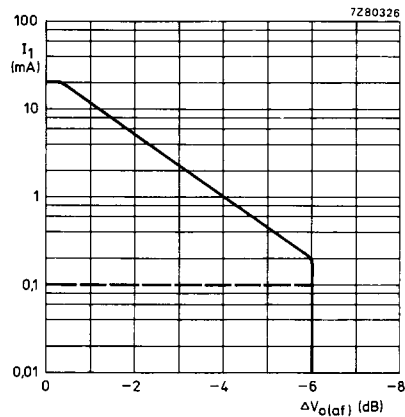


Fig. 14 Muting indicator current;  $V_p = 8,5$  to 15 V;  $V_{PL} = 14$  V.

————  $R_{bias1} = 680 \Omega$

-----  $R_{bias1} = \text{matched}$

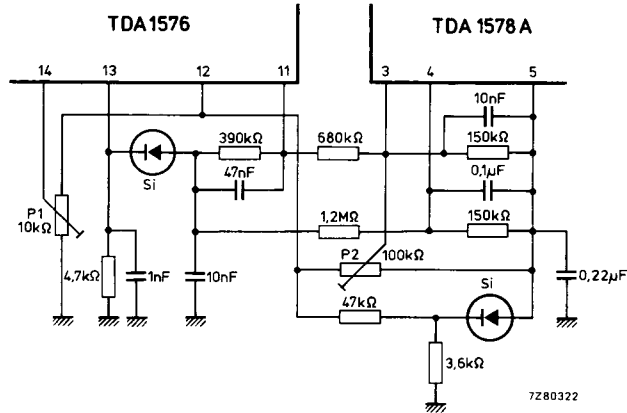


Fig. 15 Application information for external circuitry to provide external mono/stereo and muting control.

Adjustment recommendations:

at  $V_{i(hf)} = 100 \mu V$  with P1 to  $\alpha = 6 \text{ dB}$  (channel separation),  
 at  $V_{i(hf)} = 15 \mu V$  with P2 to  $V_{o(af)} = -3 \text{ dB}$ .

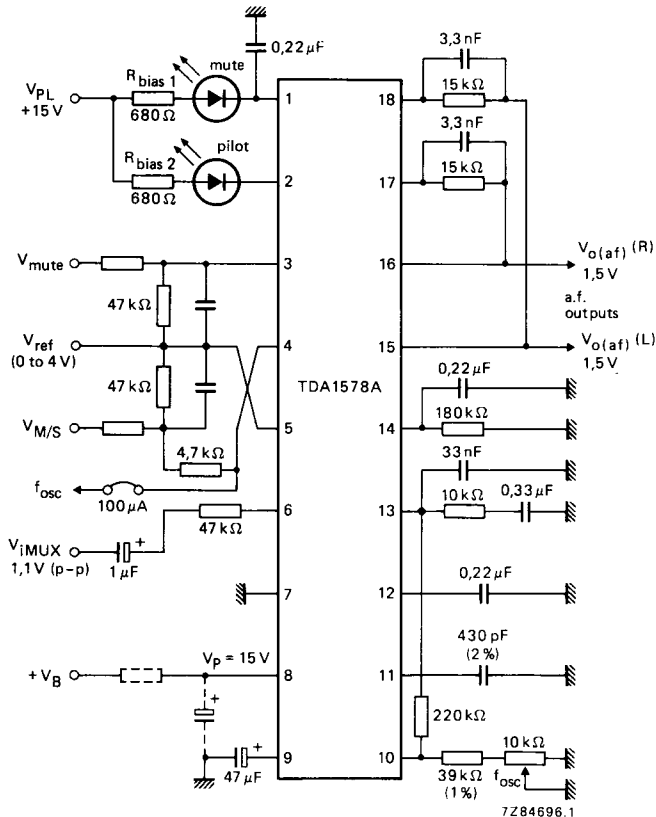


Fig. 16 Typical application circuit using TDA1578A for  $V_p = 15 \text{ V}$ .